

(12) INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

(19) World Intellectual Property  
Organization  
International Bureau



(43) International Publication Date  
17 June 2004 (17.06.2004)

PCT

(10) International Publication Number  
**WO 2004/050799 A1**

(51) International Patent Classification<sup>7</sup>: **C10G 2/00**,  
C07C 1/04, B01J 19/24

(21) International Application Number:  
PCT/GB2003/005198

(22) International Filing Date:  
27 November 2003 (27.11.2003)

(25) Filing Language: English

(26) Publication Language: English

(30) Priority Data:  
PCT/GB02/005443  
2 December 2002 (02.12.2002) GB  
0314790.7 25 June 2003 (25.06.2003) GB

(71) Applicant (for all designated States except US): **GTL MICROSYSTEMS AG [CH/CH]**; Rigmstrasse 184, CH-6340 Baar (CH).

(72) Inventors; and

(75) Inventors/Applicants (for US only): **BOWE, Michael**,

Joseph [GB/GB]; 17 Balmoral Road, New Longton, Preston, Lancashire PR4 4JJ (GB). LEE-TUFFNELL, Clive, Derek [GB/GB]; 40 Martin Close, Poole, Dorset BH17 7XS (GB).

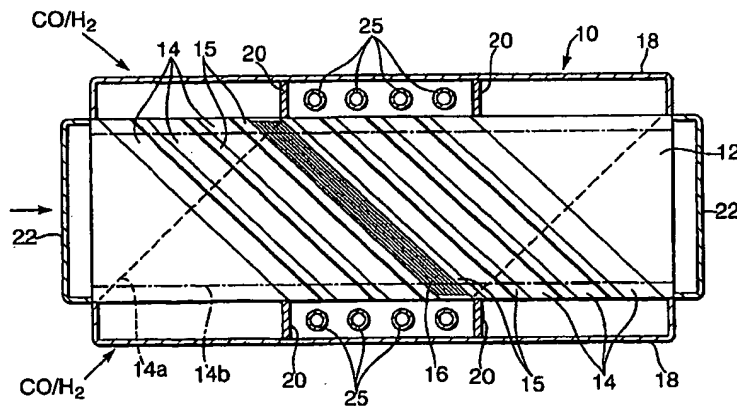
(74) Agents: **MANSFIELD, Peter**, Turquand et al.; c/o Accentus plc, Patents Dept, 329 Harwell, Didcot, Oxfordshire OX11 0QJ (GB).

(81) Designated States (national): AE, AG, AL, AM, AT, AU, AZ, BA, BB, BG, BR, BY, BZ, CA, CH, CN, CO, CR, CU, CZ, DE, DK, DM, DZ, EC, EE, ES, FI, GB, GD, GE, GH, GM, HR, HU, ID, IL, IN, IS, JP, KE, KG, KP, KR, KZ, LC, LK, LR, LS, LT, LU, LV, MA, MD, MG, MK, MN, MW, MX, MZ, NI, NO, NZ, OM, PG, PH, PL, PT, RO, RU, SC, SD, SE, SG, SK, SL, SY, TJ, TM, TN, TR, TT, TZ, UA, UG, US, UZ, VC, VN, YU, ZA, ZM, ZW.

(84) Designated States (regional): ARIPO patent (BW, GH, GM, KE, LS, MW, MZ, SD, SL, SZ, TZ, UG, ZM, ZW), Eurasian patent (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European patent (AT, BE, BG, CH, CY, CZ, DE, DK, EE, ES, FI, FR, GB, GR, HU, IE, IT, LU, MC, NL, PT, RO, SE, SI, SK, TR), OAPI patent (BF, BJ, CF, CG, CI, CM, GA, GN, GQ, GW, ML, MR, NE, SN, TD, TG).

[Continued on next page]

(54) Title: CATALYTIC REACTOR AND PROCESS



(57) Abstract: Fischer-Tropsch synthesis is performed using a compact catalytic reactor unit (10) defining channels in which is a gas-permeable catalyst structure (16), the channels extending between headers (18). The synthesis occurs in at least two stages, as the reactor unit provides at least two successive channels (14, 14a) for the Fischer-Tropsch synthesis connected by a header, the gas flow velocity through the first channel being sufficiently high that no more than 65% of the carbon monoxide undergoes conversion. The gases are cooled (25) in the header between the two stages, so as to condense water vapour, and then pass through the second channel at a sufficiently high gas flow velocity that no more than 65% of the remaining carbon monoxide undergoes conversion. This lowers the partial pressure of water vapour and so suppresses oxidation of the catalyst.

WO 2004/050799 A1

**Declarations under Rule 4.17:**

- as to applicant's entitlement to apply for and be granted a patent (Rule 4.17(ii)) for the following designations AE, AG, AL, AM, AT, AU, AZ, BA, BB, BG, BR, BY, BZ, CA, CH, CN, CO, CR, CU, CZ, DE, DK, DM, DZ, EC, EE, ES, FI, GB, GD, GE, GH, GM, HR, HU, ID, IL, IN, IS, JP, KE, KG, KP, KR, KZ, LC, LK, LR, LS, LT, LU, LV, MA, MD, MG, MK, MN, MW, MX, MZ, NI, NO, NZ, OM, PG, PH, PL, PT, RO, RU, SC, SD, SE, SG, SK, SL, SY, TJ, TM, TN, TR, TT, TZ, UA, UG, UZ, VC, VN, YU, ZA, ZM, ZW, ARIPO patent (BW, GH, GM, KE, LS, MW, MZ, SD, SL, SZ, TZ, UG, ZM, ZW), Eurasian patent (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European patent (AT, BE, BG, CH, CY, CZ, DE, DK,

EE, ES, FI, FR, GB, GR, HU, IE, IT, LU, MC, NL, PT, RO, SE, SI, SK, TR), OAPI patent (BF, BJ, CF, CG, CI, CM, GA, GN, GQ, GW, ML, MR, NE, SN, TD, TG)

- as to the applicant's entitlement to claim the priority of the earlier application (Rule 4.17(iii)) for all designations
- of inventorship (Rule 4.17(iv)) for US only

**Published:**

- with international search report
- before the expiration of the time limit for amending the claims and to be republished in the event of receipt of amendments

For two-letter codes and other abbreviations, refer to the "Guidance Notes on Codes and Abbreviations" appearing at the beginning of each regular issue of the PCT Gazette.

### Catalytic reactor and process

This invention relates to a chemical process, and to catalytic reactors suitable for use in performing the  
5 process.

A process is described in WO 01/51194 (Accentus plc) in which methane is reacted with steam, to generate carbon monoxide and hydrogen in a first catalytic  
10 reactor; the resulting gas mixture is then used to perform Fischer-Tropsch synthesis in a second catalytic reactor. The overall result is to convert methane to hydrocarbons of higher molecular weight, which are usually liquid or solid under ambient conditions. The  
15 two stages of the process, steam/methane reforming and Fischer-Tropsch synthesis, require different catalysts, and catalytic reactors are described for each stage. The catalytic reactors enable heat to be transferred to or from the reacting gases, respectively, as the reactions  
20 are respectively endothermic and exothermic; the heat required for steam/methane reforming is provided by gas combustion. A known catalyst for the Fischer-Tropsch synthesis utilises small particles of cobalt on a ceramic support, but it has been found that this catalyst can  
25 suffer oxidation or an irreversible reaction with the ceramic support in the presence of water vapour, with a resultant decrease in activity. An improved way of performing this process has now been found.

30 According to the present invention there is provided a process for performing Fischer-Tropsch synthesis using at least one compact catalytic reactor unit defining channels for the Fischer-Tropsch synthesis reaction in which there is a gas-permeable catalyst structure,  
35 wherein a carbon-monoxide-containing gas undergoes Fisher-Tropsch synthesis in at least two successive

- 2 -

stages, the gas flow velocity in the first stage being sufficiently high that no more than 70% of the carbon monoxide undergoes the synthesis reaction in the first stage, the gases being cooled between the successive stages so as to condense water vapour, and the gas flow velocity in the second stage being sufficiently high that no more than 70% of the remaining carbon monoxide undergoes the synthesis reaction in the second stage.

10            Preferably in both the first stage and the second stage the space velocity is above 1000 /hr, but preferably no greater than 15000 /hr. Preferably the process is operated so that water vapour does not exceed 20 mole%. Preferably, in each stage, no more than 65% of  
15 the carbon monoxide undergoes conversion.

The space velocity, in this specification, is defined as the volume flow rate of the gases supplied to the reactor (measured at STP), divided by the void volume of the reactor. Thus, if the reactor is at 210°C and a pressure of 2.5 MPa, a space velocity of 5000 /hr corresponds to a gas flow (at operating conditions) of about 354 times the void volume per hour, and so to a residence time of about 10s.

25            Thus the invention also provides a process for performing Fischer-Tropsch synthesis on a gas containing hydrogen and carbon monoxide using at least one compact catalytic reactor unit defining channels for the Fischer-Tropsch synthesis reaction in which there is a gas-permeable catalyst structure, wherein the synthesis reaction is performed in at least two successive stages, at a sufficiently high gas flow velocity that water vapour does not exceed 20 mole%, and that between  
30 successive stages the gases are cooled so as to condense water vapour.  
35

- 3 -

The invention also provides an apparatus for performing such a Fischer-Tropsch synthesis. This may be a compact catalytic reactor unit incorporating headers that connect successive flow channels, the headers  
5 enclosing means to condense water vapour and to remove condensed liquids from the header. The catalytic reactor unit preferably comprises a plurality of metal sheets arranged as a stack and bonded together to define  
10 channels for the Fischer-Tropsch synthesis alternating with channels for a heat exchange fluid. Preferably the temperature in the synthesis channels is above 190°C, for example 200°C. Corrugated or dimpled foils, metal meshes, or corrugated or pleated metal felt sheets may be used as the substrate of the catalyst structure within the flow  
15 channels to enhance heat transfer and catalyst surface area.

It will be appreciated that the materials of which the reactor are made are subjected to a corrosive  
20 atmosphere in use. The reactor may be made of a metal such as an aluminium-bearing ferritic steel, for example it might comprise iron with 15% chromium, 4% aluminium, and 0.3% yttrium (eg Fecralloy (TM)). When this metal is heated in air it forms an adherent oxide coating of  
25 alumina which protects the alloy against further oxidation; this oxide layer also protects the alloy against corrosion. Where this metal is used as a catalyst substrate, and is coated with a ceramic layer into which a catalyst material is incorporated, the  
30 alumina oxide layer on the metal is believed to bind with the oxide coating, so ensuring the catalytic material adheres to the metal substrate. Other stainless steels may also be used. The sheets defining the channels may alternatively be of aluminium.

35

The invention will now be further and more

- 4 -

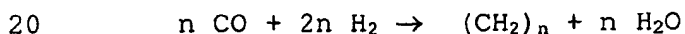
particularly described, by way of example only, and with reference to the accompanying drawings, in which:

Figure 1 shows a sectional view of a reactor  
5 suitable for performing Fischer-Tropsch synthesis,  
showing a plate in plan; and

Figure 2 shows a modification, of the reactor of  
figure 1.

10

The invention relates to Fischer-Tropsch synthesis,  
which may form part of a process for converting methane  
to longer chain hydrocarbons. Fischer-Tropsch synthesis  
is a reaction between carbon monoxide and hydrogen, and  
15 this gas mixture may for example be generated by  
steam/methane reforming. In Fischer-Tropsch synthesis  
the gases react to generate a longer chain hydrocarbon,  
that is to say:



which is an exothermic reaction, occurring at an elevated  
temperature, typically between 190 and 350°C, for example  
210°C, and an elevated pressure typically between 2 MPa  
25 and 4 MPa, for example 2.5 MPa, in the presence of a  
catalyst such as iron, cobalt or fused magnetite, with a  
promoter. The exact nature of the organic compounds  
formed by the reaction depends on the temperature, the  
pressure, and the catalyst, as well as the ratio of  
30 carbon monoxide to hydrogen.

A preferred catalyst comprises a coating of gamma-  
alumina of specific surface area 140 - 450 m<sup>2</sup>/g with about  
10-40% (by weight compared to the weight of alumina) of  
35 cobalt, and with a ruthenium/platinum promoter, the  
promoter being between 0.01% to 10% of the weight of the

- 5 -

cobalt. There may also be a basicity promoter such as gadolinium oxide. The activity and selectivity of the catalyst depends upon the degree of dispersion of cobalt metal upon the support, the optimum level of cobalt dispersion being typically in the range 0.1 to 0.2, so that between 10% and 20% of the cobalt metal atoms present are at a surface. The larger the degree of dispersion, clearly the smaller must be the cobalt metal crystallite size, and this is typically in the range 5-15 nm. Cobalt particles of such a size provide a high level of catalytic activity, but may be oxidised in the presence of water vapour, and this leads to a dramatic reduction in their catalytic activity. The extent of this oxidation depends upon the proportions of hydrogen and water vapour adjacent to the catalyst particles, and also their temperature, higher temperatures and higher proportions of water vapour both increasing the extent of oxidation.

Referring now to figure 1 a reactor 10 for Fischer-Tropsch synthesis comprises a stack of Fecralloy steel plates 12, each plate being generally rectangular, 450 mm long and 150 mm wide and 6 mm thick, these dimensions being given only by way of example. On the upper surface of each such plate 12 are rectangular grooves 14 of depth 5 mm separated by lands 15 (eight such grooves being shown), but there are three different arrangements of the grooves 14. In the plate 12 shown in the drawing the grooves 14 extend diagonally at an angle of 45° to the longitudinal axis of the plate 12, from top left to bottom right as shown. In a second type of plate 12 the grooves 14a (as indicated by broken lines) follow a mirror image pattern, extending diagonally at 45° from bottom left to top right as shown. In a third type of plate 12 the grooves 14b (as indicated by chain dotted lines) extend parallel to the longitudinal axis.

- 6 -

The plates 12 are assembled in a stack, with each of the third type of plate 12 (with the longitudinal grooves 14b) being between a plate with diagonal grooves 14 and a plate with mirror image diagonal grooves 14a, and after assembling many plates 12 the stack is completed with a blank rectangular plate. The plates 12 are compressed together and subjected to a heat treatment to bring about diffusion bonding or they are brazed together, so they are sealed to each other. Corrugated Fecralloy alloy foils 16 (only one is shown) 50 microns thick coated with a ceramic coating impregnated with a catalyst material, of appropriate shapes and with corrugations 5 mm high, can be slid into each such diagonal groove 14 or 14a.

More preferably pairs of corrugated catalyst-coated foils 16 with corrugations about 2.4 mm high are stacked together with a flat catalyst-coated foil between them, and spot welded together, before being slid into the grooves 14 or 14a.

Header chambers 18 are welded to the stack along each side, each header 18 defining three compartments by virtue of two fins 20 that are also welded to the stack. The fins 20 are one third of the way along the length of the stack from each end, and coincide with a land 15 (or a portion of the plates with no groove) in each plate 12 with diagonal grooves 14 or 14a. Coolant headers 22 in the form of rectangular caps are welded onto the stack at each end, communicating with the longitudinal grooves 14b. In a modification (not shown), in place of each three-compartment header 18 there might instead be three adjacent header chambers, each being a rectangular cap like the headers 22. Within each of the central compartments of the headers 18 there are coolant tubes 25 that extend the entire height of the stack. At the base

- 7 -

of each of these central compartments is an outlet duct (not shown) through which liquids condensing onto the tubes 25 can emerge. For use, the reactor 10 is arranged with the plates 12 in substantially horizontal planes so  
5 that the coolant tubes 25 are substantially vertical.

In use of the reactor 10 the mixture of carbon monoxide and hydrogen is supplied to the compartments of both headers 18 at one end (the left hand end as shown)  
10 of the stack, and so gases produced by Fischer-Tropsch synthesis emerge through the compartments of both headers 18 at the right hand end as shown. The flow path for the mixture supplied to the top-left header compartment (as shown), for example, is through the diagonal grooves 14  
15 into the bottom-middle header compartment, and then to flow through the diagonal grooves 14a in other plates in the stack into the top-right header compartment. A coolant is supplied to the header 22 at the same end of the stack, to maintain the temperature within the reactor  
20 10 at about 210°C, so that the coolant is at its lowest temperature at the area where heat generation is at its maximum during the first stage. Hence the flows of the reacting gases and the coolant are at least partially co-current. The intention is to approach isothermal  
25 conditions throughout the reactor 10; this has the advantage of minimising the risk of any wax (i.e. very long chain hydrocarbon) blocking the flow channels towards the outlet from the reaction channels if the local temperature drops below about 190°C. (If wax  
30 deposits occur, they may be removed by raising the coolant temperature by between 5° and 15°C, and feeding hydrogen-rich tail gas through the reactor.) The flow rate (space velocity) of the reacting gases is in the range 1000 - 15000 /hr, so as to ensure that the  
35 conversion of carbon monoxide is only about 60% or less by the time the gases reach the middle compartments of

- 8 -

the headers 18.

The coolant tubes 25 are supplied with coolant at a different temperature so that they are cooler, for example at 150°C (which is below the boiling point of water at the pressure in the reactor). Consequently water vapour (and some of the longer-chain hydrocarbons) condense on the outer surface of the coolant tubes 25, and runs down those tubes 25 to emerge from the outlet duct (not shown) at the bottom of the stack. This significantly reduces the partial pressure of water vapour in the gas mixture that flows on into the next set of diagonal grooves 14 or 14a. The result is that the Fischer-Tropsch synthesis takes place in two successive stages - the first stage being as the gas flows from the inlet compartments of the headers 18 to the middle compartments; and the second stage being as the gas flows from the middle compartments to the outlet compartments - and at least part of the water vapour generated in the first stage is removed from the gas stream before it enters the second stage.

It will be appreciated that the reactor 10 may be modified in various ways, and that in particular the plates 12 may be of different thicknesses. For example the plates 12 defining the diagonal grooves 14 and 14a in which Fischer-Tropsch synthesis takes place might be 10 mm thick with grooves 9 mm deep, while the plates 12 with longitudinal grooves 14b for the coolant might be only 4 mm thick with 3 mm deep grooves. In this case the corrugated foils 16 might be replaced by a stack of say three or four corrugated foils which may be spot welded together so the overall height is 9 mm. Such deeper grooves provide an advantage if any waxy material is produced, as they are less vulnerable to blockage. Channels greater than about 2 mm deep improve the bulk

- 9 -

transport properties of the corrugated catalyst insert 16; in the case of Fischer-Tropsch synthesis this enables efficient drainage and removal of liquid products, and transfer of reactant gases to the surface of the catalyst. The pitch or pattern of the corrugated foils 16 may vary along a reactor channel 14 or 14a to adjust catalytic activity, and hence provide for control over the temperatures or reaction rates at different points in the reactor 10. Furthermore the diagonal grooves may decrease in width, and possibly also depth, along their length, so as to vary the fluid flow conditions, and the heat or mass transfer coefficients.

During the synthesis reaction the gas volume decreases, and by appropriate tapering of the channels 14 the gas velocity may be maintained as the reaction proceeds, to maintain the target conversion. An alternative way of maintaining the gas velocity is to decrease the number of flow channels, as shown in figure 2, to which reference is now made. This shows a view corresponding to that of figure 1. The only difference is that the diagonal grooves 14 (and 14a) defining the second stage of the Fischer-Tropsch synthesis, that is to say the grooves 14 (and 14a) between the middle compartment and the right hand compartment of the headers 18, are separated by wider lands 30, so that there are only three such grooves in each plate 12.

It will also be appreciated that a modified reactor might provide more stages, for example being a three stage Fischer-Tropsch reactor, the headers 18 defining four successive compartments along each side of the reactor, and with condenser tubes 25 in each of the two middle compartments. The overall conversion may be substantially the same, for example two 60% conversion stages and three 50% conversion stages would each provide

- 10 -

an overall conversion above 80%.

Removal of the water vapour and the lower boiling point hydrocarbons onto the condenser tubes 25 not only lowers the partial pressure of water vapour and so suppresses the oxidation of the catalyst, but has the further benefit of removing at least some of those hydrocarbons that would form a liquid layer on the catalyst structure. Any such a liquid layer inhibits contact of the gas mixture with the catalyst particles and inhibits diffusion of the product hydrocarbons away from the catalyst particles, so removal of the hydrocarbons liquid minimises these diffusional resistances.

In figures 1 and 2 only four condenser tubes 25 are shown in each middle compartment, but it will be appreciated that there might be a different number of tubes, for example ten or more. And to enhance heat transfer each tube 25 may be provided with fins, preferably fins extending longitudinally so that flow of condensed liquid down the tube 25 is not impeded. Not only does water vapour condense on the tubes, but any liquid droplets entrained with the gas flow tend to impact with the surface of the tubes 25 and so are disengaged from the gas flow. As an alternative to the heat exchanger tubes 25 or other heat transfer surfaces, a spray condenser system may be provided within the middle compartments of the headers 18, which might use as the coolant fluid recycled products from the Fischer-Tropsch synthesis at about 150°C. This would be particularly beneficial if there is a risk of wax deposits fouling the heat exchanger surfaces.

Alternatively the cooling and condensation may be carried out separate from and outside the reactor. For

- 11 -

example three reactors 10 as shown in Figure 1 but without the cooling tubes 25 in the header might be arranged to carry gas flows in parallel, the conversion of CO being restricted to below 65% by controlling the  
5 reaction temperature and space velocity. The outlet gases from the three reactors are connected via a manifold to a condenser unit in which the water vapour and liquid hydrocarbon product is condensed. The remaining gases, with lowered water partial pressure,  
10 might then be supplied to a single such reactor 10 (again without the cooling tubes 25), so that again about 60% of the residual unreacted CO undergoes the synthesis reaction. The decrease in gas volume between the first stage and the second stage - because much of the gas has  
15 undergone synthesis and formed a liquid - is accommodated by reducing the number of reactor units from three to one, so as to maintain a high flow velocity.

Additional benefits of the high gas flow velocity  
20 are a reduction in the temperature variation across the reaction channels, by helping to redistribute the heat from the exothermic reactions at the surface of the catalyst into the gas phase. It also helps to entrain the liquid reaction products into the gas flow and to  
25 keep the catalyst surface free of waxy deposits.

Claims

1. A process for performing Fischer-Tropsch synthesis using at least one compact catalytic reactor unit (10) defining channels (14, 14a) for the Fischer-Tropsch synthesis reaction in which there is a gas-permeable catalyst structure (16), characterized in that a carbon monoxide-containing gas undergoes Fischer-Tropsch synthesis in at least two successive stages, the gas flow velocity in the first stage being sufficiently high that no more than 70% of the carbon monoxide undergoes the synthesis reaction in the first stage, the gases being cooled (25) between the successive stages so as to condense water vapour, and the gas flow velocity in the second stage being sufficiently high that no more than 70% of the remaining carbon monoxide undergoes the synthesis reaction in the second stage.
2. A process as claimed in claim 1 performed using a single reactor unit (10), wherein each stage of the synthesis reaction takes place in a set of channels (14, 14a) within the reactor unit, and the gases are cooled (25) within a header (18) between successive stages.
3. A process as claimed in claim 1 or claim 2 wherein a carbon monoxide-containing gas stream flows through a plurality of first channels (14, 14a) in parallel in the first stage, and then through a plurality of second channels (14, 14a) in parallel in the second stage, the cross-sectional area of the plurality of second channels (14, 14a) being less than that of the plurality of first channels (14, 14a).
4. A process as claimed in claim 3 wherein the number of second channels (14, 14a) is less than the number of first channels (14, 14a).

- 13 -

5. A process as claimed in any one of the preceding claims wherein in both the first stage and the second stage the space velocity is above 1000 /hr.
- 5 6. A process as claimed in claim 5 wherein, in both the first stage and the second stage the space velocity is no greater than 15000 /hr.
7. A process as claimed in any one of the preceding  
10 claims wherein water vapour does not exceed 20 mole%.
8. A process as claimed in any one of the preceding claims wherein the gas flow velocity through both the first stage and the second stage is sufficiently high  
15 that no more than 65% of the carbon monoxide undergoes the synthesis reaction.
9. A process for performing Fischer-Tropsch synthesis on a gas containing hydrogen and carbon monoxide using at  
20 least one compact catalytic reactor unit (10) defining channels (14, 14a) for the Fischer-Tropsch synthesis in which there is a gas-permeable catalyst structure(16), wherein the synthesis is performed in at least two successive stages, at a sufficiently high gas flow  
25 velocity that water vapour does not exceed 20 mole%, and that between successive stages the gases are cooled (25) so as to condense water vapour.
10. Apparatus for performing a Fischer-Tropsch synthesis  
30 as claimed in any one of the preceding claims, comprising at least one compact catalytic reactor unit (10) defining channels (14, 14a) for the Fischer-Tropsch synthesis reaction in which there is a gas-permeable catalyst structure (16), connecting means (18) communicating  
35 between successive sets of channels (14, 14a), and cooling means (25) within the connecting means to

- 14 -

condense water vapour and to remove condensed liquids from the gas flow.

11. Apparatus as claimed in claim 10 wherein the  
5 successive sets of channels (14, 14a) are in the same reactor unit (10), and the connecting means (18) is a header.
12. Apparatus as claimed in claim 10 or claim 11 wherein  
10 the cross-sectional area of the flow channels (14, 14a) carrying flow out of the connecting means (18) is less than the cross-sectional area of the flow channels (14, 14a) carrying flow into the connecting means (18).
13. Apparatus as claimed in any one of claims 10 to 12  
15 wherein the number of flow channels (14, 14a) carrying flow out of the connecting means (18) is less than the number of flow channels (14, 14a) carrying flow into the connecting means (18).
14. Apparatus as claimed in any one of claims 10 to 13  
20 also comprising means (14b) to ensure the temperature in the synthesis channels (14, 14a) does not exceed 210°C.

1/1

Fig.1.

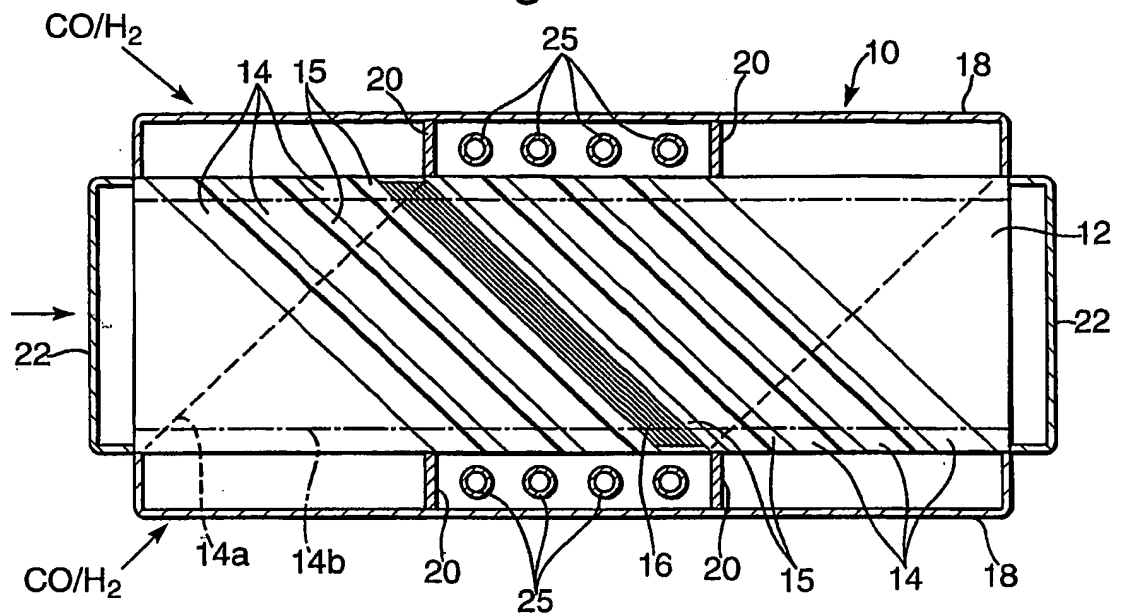
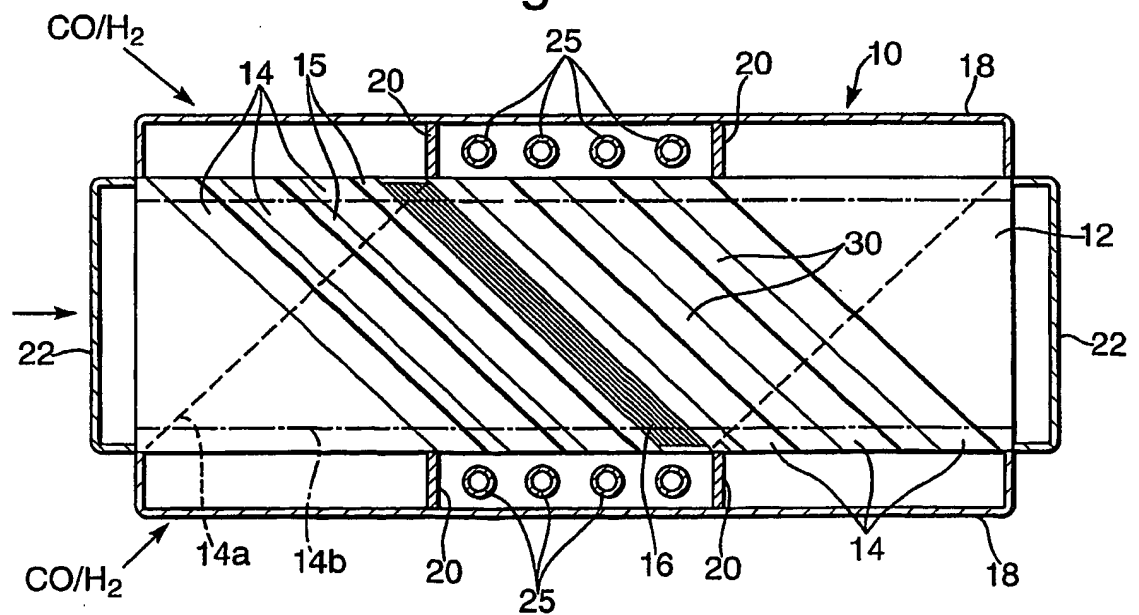


Fig.2.



# INTERNATIONAL SEARCH REPORT

Int      Application No  
PCT/GB 03/05198

**A. CLASSIFICATION OF SUBJECT MATTER**  
IPC 7    C10G2/00    C07C1/04    B01J19/24

According to International Patent Classification (IPC) or to both national classification and IPC

**B. FIELDS SEARCHED**

Minimum documentation searched (classification system followed by classification symbols)  
IPC 7    C10G    C07C    B01J

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EPO-Internal

**C. DOCUMENTS CONSIDERED TO BE RELEVANT**

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	FR 2 824 755 A (PHYSIQUES ET CHIMIQUES) 22 November 2002 (2002-11-22) page 8, paragraph 1 page 22, paragraph 3 - paragraph 4; figure 7	1-14
A	US 4 199 523 A (ROTTIG WALTER) 22 April 1980 (1980-04-22) column 2, paragraphs 4,5; example 1 column 3, paragraph 6	1-14
P,A	WO 03/033131 A (BOWE MICHAEL JOSEPH ;ACCENTUS PLC (GB); LEE-TUFFNELL CLIVE DEREK ()) 24 April 2003 (2003-04-24) claims 1-11; figure 2	1-14

☐ Further documents are listed in the continuation of box C.

☒ Patent family members are listed in annex.

**\* Special categories of cited documents :**

- "A" document defining the general state of the art which is not considered to be of particular relevance
- "E" earlier document but published on or after the international filing date
- "L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)
- "O" document referring to an oral disclosure, use, exhibition or other means
- "P" document published prior to the international filing date but later than the priority date claimed

- "T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
- "X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
- "Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.
- "&" document member of the same patent family

Date of the actual completion of the international search

29 April 2004

Date of mailing of the international search report


10/05/2004

Name and mailing address of the ISA  
European Patent Office, P.B. 5818 Patentlaan 2  
NL - 2280 HV Rijswijk  
Tel. (+31-70) 340-2040, Tx. 31 651 epo nl,  
Fax: (+31-70) 340-3018

Authorized officer

Gilliquet, J-N

# INTERNATIONAL SEARCH REPORT

Int  Application No  
PCT/GB 03/05198

Patent document cited in search report		Publication date	Patent family member(s)		Publication date
FR 2824755	A	22-11-2002	FR	2824755 A1	22-11-2002
US 4199523	A	22-04-1980	DE	2518982 A1	11-11-1976
			AU	498400 B2	08-03-1979
			AU	1322476 A	27-10-1977
			BE	840969 A1	21-10-1976
			CA	1053265 A1	24-04-1979
			DD	123881 A5	19-01-1977
			FR	2309497 A1	26-11-1976
			GB	1490494 A	02-11-1977
			JP	1006548 C	31-07-1980
			JP	51131808 A	16-11-1976
			JP	54043481 B	20-12-1979
			NL	7509662 A ,B,	02-11-1976
			ZA	7602412 A	27-04-1977
WO 03033131	A	24-04-2003	WO	03033131 A1	24-04-2003